



# LIGHTING SCIENCES CANADA LTD.

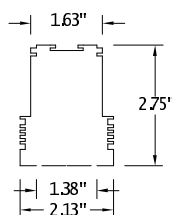
160 Frobisher Drive, Unit 5, Waterloo, Ontario, Canada N2V 2B1  
Tel: (519) 746-3140 Fax: (519) 746-3156 lsc@lightingsciences.ca

CERTIFIED TEST REPORT NO. LSC E757

RAB DESIGN LINEAR LED LUMINAIRE CAT. NO. RD-L1-8-WHT-M-500mm  
WITH INDIVIDUAL LED MEDIUM LENS OPTICS  
EIGHT WHITE PHILIPS 1.2W LEDS. LUMEN OUTPUT = 592 LMS.

## FLOODLIGHT SUMMARY:

FIELD ANGLE	42.1H X 43.6V
(BASED ON 10% OF MAX. CP.)	
BEAM ANGLE	20.3H X 21.0V
(BASED ON 50% OF MAX. CP.)	
NEMA TYPE	3H X 3V
MAX. CANDLEPOWER	3136 CANDELA
MAX. CP. VERT. ANGLE	-1.0 DEGREES
MAX. CP. HORIZ. ANGLE	.0 DEGREES
AVG. MAX. CANDLEPOWER	2820 CANDELA
FIELD FLUX	472.6 LUMENS
FIELD EFFICACY	45.9 LMS/WATT
BEAM FLUX	260.6 LUMENS
BEAM EFFICACY	25.3 LMS/WATT
TOTAL FLUX	592.3 LUMENS
TOTAL EFFICACY	57.5 LMS/WATT



PREPARED FOR:

RAB DESIGN LIGHTING INC.  
TORONTO, ONTARIO

CERTIFIED BY:

*Charles Lison*

DATE: Jan 28 2011

The above tabulation is computed in accordance with IES publication no. LM-35-1989, and defines the beam from the 50% maximum candlepower points and the field from the 10% maximum candlepower points. LM-35-1989 supersedes the 1970 document which defines the beam from the 10% maximum candlepower points.

Laboratory result may not be representative of field performance.  
ABSOLUTE PHOTOMETRY TAKEN.

LIGHTING SCIENCES CANADA LTD.  
160 FROBISHER DRIVE, UNIT 5  
WATERLOO, ONTARIO

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CANDLEPOWER TRACE THROUGH ORIGIN  
VERTICAL TRACE                      CANDELA                      HORIZONTAL TRACE

ANGLE	CANDLEPOWER	ANGLE	CANDLEPOWER	ANGLE	CANDLEPOWER	ANGLE	CANDLEPOWER
30.0	74.	.0	3104.	30.0	79.	.0	3104.
29.0	85.	-1.0	3137.	29.0	91.	-1.0	3096.
28.0	99.	-2.0	3095.	28.0	105.	-2.0	3027.
27.0	115.	-3.0	3008.	27.0	123.	-3.0	2918.
26.0	136.	-4.0	2884.	26.0	144.	-4.0	2773.
25.0	158.	-5.0	2729.	25.0	168.	-5.0	2598.
24.0	186.	-6.0	2553.	24.0	196.	-6.0	2402.
23.0	218.	-7.0	2366.	23.0	229.	-7.0	2192.
22.0	256.	-8.0	2171.	22.0	268.	-8.0	1980.
21.0	301.	-9.0	1977.	21.0	314.	-9.0	1774.
20.0	352.	-10.0	1787.	20.0	368.	-10.0	1575.
19.0	412.	-11.0	1604.	19.0	431.	-11.0	1389.
18.0	480.	-12.0	1433.	18.0	504.	-12.0	1218.
17.0	560.	-13.0	1274.	17.0	589.	-13.0	1061.
16.0	651.	-14.0	1125.	16.0	686.	-14.0	922.
15.0	756.	-15.0	991.	15.0	796.	-15.0	796.
14.0	878.	-16.0	867.	14.0	922.	-16.0	686.
13.0	1014.	-17.0	754.	13.0	1061.	-17.0	589.
12.0	1166.	-18.0	654.	12.0	1218.	-18.0	504.
11.0	1336.	-19.0	566.	11.0	1389.	-19.0	431.
10.0	1521.	-20.0	486.	10.0	1575.	-20.0	368.
9.0	1715.	-21.0	417.	9.0	1774.	-21.0	314.
8.0	1915.	-22.0	358.	8.0	1980.	-22.0	268.
7.0	2119.	-23.0	307.	7.0	2192.	-23.0	229.
6.0	2322.	-24.0	261.	6.0	2402.	-24.0	196.
5.0	2512.	-25.0	224.	5.0	2598.	-25.0	168.
4.0	2687.	-26.0	192.	4.0	2773.	-26.0	144.
3.0	2825.	-27.0	164.	3.0	2918.	-27.0	123.
2.0	2926.	-28.0	140.	2.0	3027.	-28.0	105.
1.0	3025.	-29.0	121.	1.0	3096.	-29.0	91.
.0	3104.	-30.0	103.	.0	3104.	-30.0	79.

- UPPER -

- LOWER -

- RIGHT -

- LEFT -

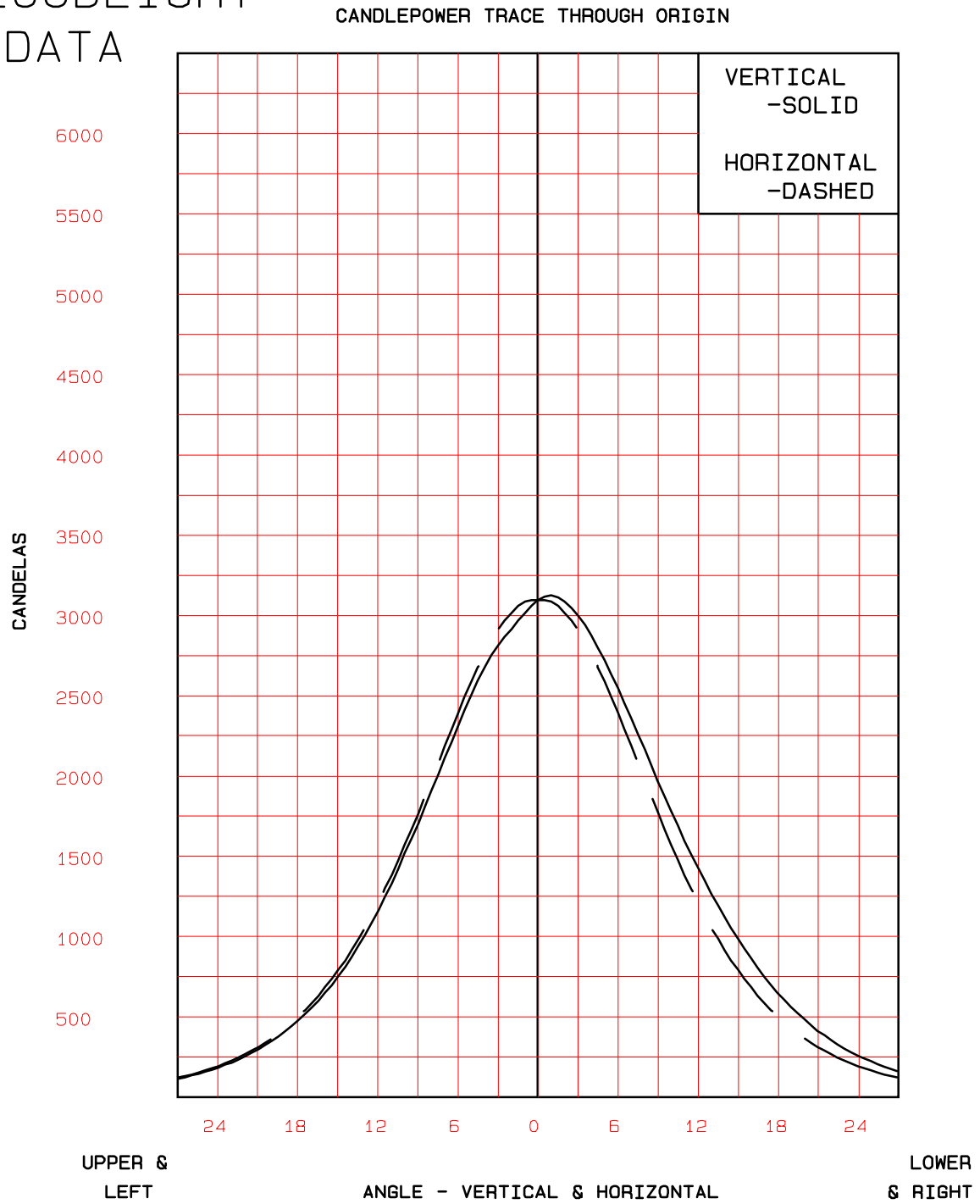
POLAR AXIS HORIZONTAL



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## FLOODLIGHT DATA





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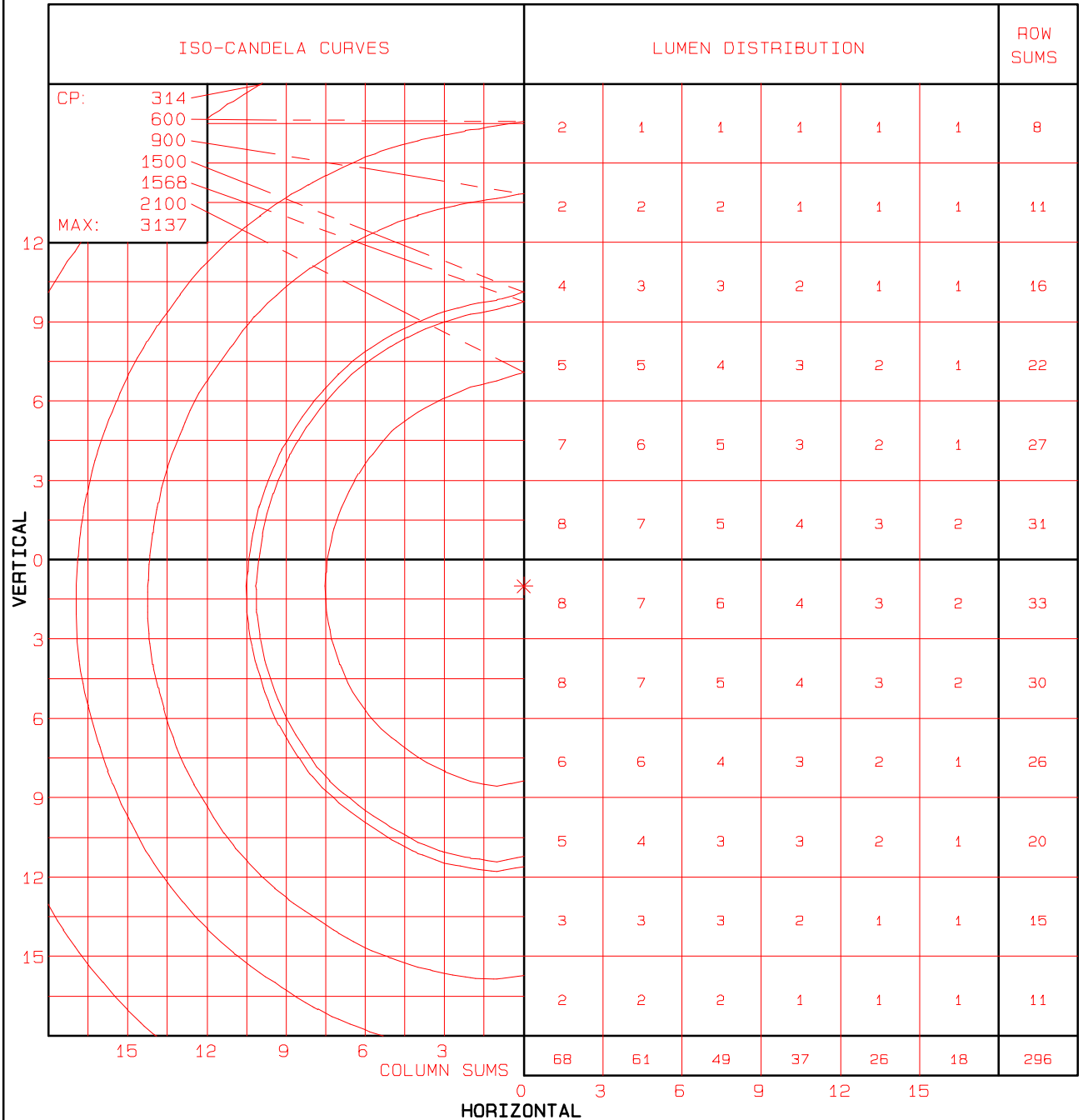
## FLOODLIGHT DATA

RAB DESIGN LINEAR LED LUMINAIRE CAT. NO. RD-L1-8-WHT-M-500mm

WITH INDIVIDUAL LED MEDIUM LENS OPTICS

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### ISOCANDELA DIAGRAM



CERTIFIED TEST REPORT NO. LSC E757  
STANDARD TABLE OF CANDELAS AND LUMENS, IN ACCORDANCE WITH IES PROCEDURES

ANGULAR DATA IS SHOWN WITH THE POLAR AXIS HORIZONTAL.

LUMINOUS INTENSITY IN CANDELAS AT CENTERS OF ZONES.

LUMINOUS FLUX IN LUMENS IN ZONES.

\*\*\*\*\* MULTIPLY CANDELAS BY 1 \*\*\*\*\*

LUMEN OUTPUT = 592 LMS.

RIGHT HAND COLUMN SHOWS LUMEN TOTAL FOR ONE SIDE ONLY, 0 TO 90 DEGREES

VERT. ANG.	HORIZONTAL ANGLE - DEGREES																		
	0.	3.	6.	9.	12.	15.	18.	21.	24.	27.	30.	33.	36.	39.	42.	45.	48.	51.	
51.		11.	10.	10.	10.	10.	10.	10.	9.	9.	9.	8.	7.	7.	6.	6.	5.	5.	.37
		.03	.03	.03	.03	.03	.03	.02	.02	.02	.02	.02	.02	.02	.01	.01	.01	.01	
48.	+		13.	13.	12.	12.	12.	11.	11.	10.	10.	9.	9.	8.	8.	7.	6.	5.	.44
		.04	.03	.03	.03	.03	.03	.03	.03	.03	.02	.02	.02	.02	.02	.01	.01	.01	
45.	+		16.	16.	15.	15.	14.	14.	13.	12.	11.	11.	10.	10.	9.	8.	8.	7.	.51
		.04	.04	.04	.04	.04	.04	.03	.03	.03	.03	.02	.02	.02	.02	.02	.01	.01	
42.	+		20.	19.	19.	18.	17.	16.	15.	14.	13.	12.	11.	11.	10.	9.	8.	8.	.61
		.06	.05	.05	.05	.05	.04	.04	.04	.04	.03	.03	.03	.02	.02	.02	.02	.01	
39.	+		27.	27.	25.	24.	22.	20.	18.	17.	15.	14.	13.	12.	11.	10.	9.	9.	.74
		.07	.07	.07	.06	.06	.05	.05	.05	.04	.04	.03	.03	.03	.02	.02	.02	.01	
36.	+		39.	38.	35.	33.	30.	26.	23.	21.	18.	16.	14.	13.	12.	11.	10.	9.	.95
		.11	.10	.10	.09	.08	.07	.06	.05	.04	.04	.03	.03	.03	.03	.02	.02	.01	
33.	+		59.	56.	52.	47.	41.	36.	31.	26.	22.	19.	16.	14.	13.	12.	10.	10.	1.26
		.16	.15	.14	.13	.11	.09	.08	.07	.05	.04	.04	.03	.03	.03	.02	.02	.02	
30.	+		90.	85.	78.	69.	60.	50.	41.	34.	27.	23.	19.	16.	14.	12.	11.	10.	1.73
		.25	.23	.21	.19	.16	.13	.11	.09	.07	.05	.04	.04	.03	.03	.03	.02	.02	
27.	+		143.	134.	121.	105.	88.	71.	57.	45.	35.	27.	22.	18.	15.	13.	12.	11.	2.47
		.39	.37	.33	.28	.23	.19	.15	.11	.09	.07	.05	.04	.03	.03	.03	.02	.02	
24.	+		229.	213.	189.	160.	129.	102.	78.	59.	45.	34.	26.	21.	17.	14.	12.	11.	3.61
		.63	.58	.51	.43	.34	.27	.20	.15	.11	.08	.06	.05	.04	.03	.03	.02	.02	
21.	=====	#																	5.33
		367.	338.	295.	243.	191.	145.	108.	79.	57.	42.	31.	24.	19.	15.	14.	12.	11.	
		1.00	.93	.80	.66	.51	.38	.28	.20	.14	.10	.07	.05	.04	.03	.03	.02	.02	
18.	+		583.	534.	455.	366.	279.	205.	146.	102.	72.	51.	37.	27.	21.	17.	14.	12.	7.86
		1.60	1.46	1.24	.99	.74	.54	.38	.26	.18	.12	.09	.06	.05	.03	.03	.02	.02	
15.	+		910.	825.	688.	537.	397.	281.	193.	131.	90.	61.	43.	31.	23.	18.	15.	13.	11.46
		2.49	2.25	1.87	1.45	1.06	.74	.50	.33	.22	.15	.10	.07	.05	.04	.03	.02	.02	
12.	+		1367.	1222.	1002.	761.	540.	371.	248.	165.	108.	72.	49.	34.	25.	19.	16.	13.	16.20
		3.75	3.34	2.72	2.05	1.44	.98	.64	.42	.27	.17	.11	.08	.05	.04	.03	.02	.02	
9.	+		1933.	1716.	1377.	1007.	703.	467.	304.	196.	127.	82.	55.	38.	27.	20.	16.	13.	21.80
		5.30	4.69	3.74	2.72	1.87	1.23	.79	.50	.31	.20	.13	.09	.06	.04	.03	.03	.02	
6.	+		2521.	2226.	1741.	1260.	854.	557.	354.	224.	142.	91.	59.	40.	28.	21.	16.	14.	27.40
		6.91	6.08	4.73	3.40	2.28	1.47	.91	.57	.35	.22	.14	.09	.06	.04	.03	.03	.02	

3.	2960.	2582.	2019.	1438.	962.	621.	391.	243.	153.	97.	63.	42.	29.	21.	17.	14.	12.	
0.	8.11	7.06	5.49	3.88	2.57	1.63	1.01	.62	.38	.23	.15	.10	.06	.04	.03	.03	.02	31.47
-3.	3067.	2693.	2106.	1500.	1003.	643.	404.	252.	157.	99.	64.	43.	30.	22.	17.	14.	12.	
-6.	8.40	7.36	5.72	4.04	2.67	1.69	1.04	.64	.39	.24	.15	.10	.06	.05	.03	.03	.02	32.71
-9.	2800.	2482.	1957.	1408.	954.	619.	391.	244.	153.	97.	63.	42.	29.	22.	17.	14.	12.	
-12.	7.67	6.78	5.32	3.79	2.54	1.63	1.01	.62	.38	.23	.15	.09	.06	.05	.03	.03	.02	30.48
-15.	2294.	2040.	1655.	1212.	841.	552.	354.	226.	143.	92.	60.	40.	29.	21.	17.	14.	12.	
-18.	6.29	5.57	4.50	3.27	2.24	1.45	.91	.57	.35	.22	.14	.09	.06	.04	.03	.03	.02	25.87
-21.	1722.	1556.	1278.	974.	688.	464.	303.	197.	127.	83.	55.	38.	27.	20.	16.	14.	12.	
-24.	4.72	4.25	3.47	2.62	1.83	1.22	.78	.50	.31	.20	.13	.09	.06	.04	.03	.03	.02	20.39
-27.	1221.	1119.	932.	728.	531.	369.	248.	165.	109.	73.	50.	35.	25.	19.	16.	13.	12.	
-30.	3.35	3.06	2.53	1.96	1.41	.97	.64	.42	.27	.18	.12	.08	.06	.04	.03	.02	.02	15.22
-33.	827.	762.	652.	517.	391.	279.	195.	133.	90.	62.	43.	31.	23.	18.	15.	13.	11.	
-36.	2.27	2.08	1.77	1.39	1.04	.73	.50	.34	.22	.15	.10	.07	.05	.04	.03	.02	.02	10.90
-39.	535.	501.	436.	352.	273.	204.	147.	104.	74.	52.	37.	27.	21.	17.	14.	12.	11.	
-42.	1.47	1.37	1.18	.95	.73	.54	.38	.26	.18	.12	.09	.06	.05	.04	.03	.02	.02	7.55
-45.	338.	320.	284.	235.	187.	144.	108.	79.	58.	42.	32.	24.	19.	16.	14.	12.	11.	
-48.	.93	.87	.77	.63	.50	.38	.28	.20	.14	.10	.07	.05	.04	.03	.03	.02	.02	5.14
-51.	211.	201.	182.	155.	126.	100.	78.	59.	45.	34.	26.	21.	17.	15.	13.	11.	10.	
-54.	.58	.55	.49	.42	.34	.26	.20	.15	.11	.08	.06	.05	.04	.03	.03	.02	.02	3.48
-57.	132.	127.	116.	102.	86.	70.	56.	45.	35.	28.	22.	18.	16.	13.	12.	11.	10.	
-60.	.36	.35	.32	.27	.23	.18	.14	.11	.09	.07	.05	.04	.03	.03	.02	.02	.02	2.39
-63.	84.	82.	76.	68.	59.	49.	41.	33.	27.	23.	19.	16.	14.	12.	11.	10.	9.	
-66.	.23	.22	.21	.18	.16	.13	.11	.08	.07	.05	.04	.04	.03	.03	.02	.02	.02	1.68
-69.	55.	54.	50.	46.	41.	35.	30.	26.	22.	19.	16.	14.	13.	12.	10.	9.	9.	
-72.	.15	.15	.14	.12	.11	.09	.08	.07	.05	.04	.04	.03	.03	.02	.02	.02	.02	1.22
-75.	37.	36.	34.	32.	29.	26.	23.	20.	18.	16.	14.	13.	12.	11.	10.	9.	8.	
-78.	.10	.10	.09	.09	.08	.07	.06	.05	.04	.04	.03	.03	.03	.02	.02	.02	.01	.92
-81.	26.	26.	25.	23.	21.	20.	18.	16.	15.	13.	12.	11.	11.	10.	9.	8.	7.	
-84.	.07	.07	.07	.06	.06	.05	.05	.04	.04	.03	.03	.03	.02	.02	.02	.02	.01	.72
-87.	19.	19.	18.	17.	16.	16.	14.	14.	13.	12.	11.	10.	9.	9.	8.	7.	6.	
-90.	.05	.05	.05	.05	.04	.04	.04	.03	.03	.03	.03	.02	.02	.02	.02	.01	.01	.58
-93.	15.	14.	14.	14.	13.	12.	12.	11.	11.	10.	10.	9.	8.	7.	7.	6.	5.	
-96.	.04	.04	.04	.04	.03	.03	.03	.03	.03	.02	.02	.02	.02	.02	.01	.01	.01	.47
-99.	11.	11.	11.	10.	10.	10.	9.	9.	9.	8.	8.	7.	7.	6.	6.	5.	4.	
-102.	.03	.03	.03	.03	.03	.03	.02	.02	.02	.02	.02	.02	.01	.01	.01	.01	.01	.38
-105.	68.	61.	49.	37.	26.	18.	12.	8.	5.	4.	2.	2.	1.	1.	1.	1.	1.	

BOTTOM ROW SHOWS LUMEN SUMMATION OF VERTICAL ZONES, +90 TO - 90 DEGREES

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SUPPLEMENTARY MEASUREMENTS AS PER IES-LM-79-08

STABILIZATION TIME: 45 MINUTES

ELECTRICAL CONSUMPTION

INPUT VOLTAGE: 120.0 VRMS  
INPUT CURRENT: 0.087 ARMS  
INPUT WATTAGE: 10.30  
POWER FACTOR: 0.987

CHROMATICITY MEASUREMENTS

CIE 1931-x: 0.301  
CIE 1931-y: 0.301  
CORRELATED COLOUR TEMPERATURE: 7667 DEG. K  
COLOUR RENDERING INDEX: 77.1%